

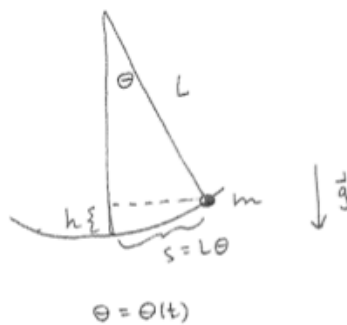
5.4 Applications of 2<sup>nd</sup> order linear homogeneous DE's with constant coefficients, to unforced spring (and related) configurations.

$$m x'' + c x' + k x = 0$$

• On Tuesday we discussed undamped oscillations,  $c = 0$ , which are described by simple harmonic motion. Today discuss damping  $c \neq 0$  in the unforced oscillator equation above, following the last two pages of Tuesday's notes. We wish to understand the overdamped, critically damped, and underdamped situations.

• Then we should have time for two (undamped) experiments, using a pendulum configuration in one, and an oscillating mass-spring configuration in the other.

① pendulum



conservative system  $KE + PE = \text{const.}$

$$\frac{1}{2} m v^2 + mgh = \text{const}$$

$$s = L\theta$$

$$v = \frac{ds}{dt} = L\theta'(t)$$

$$h = L - L \cos \theta = L(1 - \cos \theta)$$

so,  $\frac{1}{2} m L^2 (\theta'(t))^2 + mgL(1 - \cos(\theta(t))) \equiv \text{const}$

$D_t$ :  $m L^2 \theta' \theta'' + mgL(\sin \theta) \theta' \equiv 0$   
 $\underline{m L \theta'} (L \theta'' + g \sin \theta) \equiv 0$   
 $\neq 0$  except at isolated times

$\sim$  deduce eqn of motion is

linearize  $\boxed{\theta'' + \frac{g}{L} \sin \theta = 0}$

$\boxed{\theta'' + \frac{g}{L} \theta = 0}$

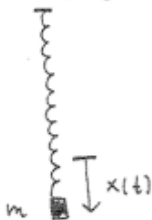
$$\omega_0 = \sqrt{\frac{g}{L}}$$

$$\theta(t) = C \cos(\omega_0 t - \alpha)$$

$\searrow$  non-linear DE  
 but  $\sin \theta = \theta - \frac{\theta^3}{3!} + \dots$

$\sin \theta \approx \theta$   $\theta$  small  
 is excellent approx  
 (alternating series test)

② hanging mass-spring:



$$m x'' = -kx$$

$$m x'' + kx = 0$$

$$\boxed{x'' + \frac{k}{m} x = 0}$$

$$\omega_0 = \sqrt{\frac{k}{m}}$$

Why don't you see gravity  $g$  in this DE?

Pendulum: measurements and prediction (we'll check these numbers).

```

> restart :
  Digits := 4 :

> L := 1.526;
  g := 9.806;
  ω := √(g/L); # radians per second
  f := evalf(ω/(2·Pi)); # cycles per second
  T := 1/f; # seconds per cycle

```

Experiment:

Mass-spring:

compute Hooke's constant:

```

> 98.7 - 83.4; #displacement from extra 50g
> k := .05·9.806 / .153; # solve k·x=m·g for k.
> m := .1; # mass for experiment is 100g
  ω := √(k/m); # predicted angular frequency
  f := evalf(ω/(2·Pi)); # predicted frequency
  T := 1/f; # predicted period

```

Experiment:

We neglected the  $KE_{spring}$ , which is small but could be adding inertia to the system and slowing down the oscillations. We can account for this:

### Improved mass-spring model

Normalize  $TE = KE + PE = 0$  for mass hanging in equilibrium position, at rest. Then for system in motion,

$$KE + PE = KE_{mass} + KE_{spring} + PE_{work}.$$

$$PE_{work} = \int_0^x k s \, ds = \frac{1}{2} k x^2, \quad KE_{mass} = \frac{1}{2} m (x'(t))^2, \quad KE_{spring} = ???$$

How to model  $KE_{spring}$  ? Spring is at rest at top (where it's attached to bar), moving with velocity  $x'(t)$  at bottom (where it's attached to mass). Assume it's moving with velocity  $\mu x'(t)$  at location which is fraction  $\mu$  of the way from the top to the mass. Then we can compute  $KE_{spring}$  as an integral with respect to  $\mu$ , as the fraction varies  $0 \leq \mu \leq 1$  :

$$KE_{spring} = \int_0^1 \frac{1}{2} (\mu x'(t))^2 (m_{spring} d\mu) \\ = \frac{1}{2} m_{spring} (x'(t))^2 \int_0^1 \mu^2 d\mu = \frac{1}{6} m_{spring} (x'(t))^2 .$$

Thus

$$TE = \frac{1}{2} \left( m + \frac{1}{3} m_{spring} \right) (x'(t))^2 + \frac{1}{2} k x^2 = \frac{1}{2} M (x'(t))^2 + \frac{1}{2} k x^2 ,$$

where

$$M = m + \frac{1}{3} m_{spring}$$

$$D_t(TE) = 0 \Rightarrow$$

$$M x'(t) x''(t) + k x(t) x'(t) = 0 . \\ x'(t) (M x'' + k x) = 0 .$$

Since  $x'(t) = 0$  only at isolated  $t$ -values, we deduce that the corrected equation of motion is

$$(M x'' + k x) = 0$$

with

$$\omega_0 = \sqrt{\frac{k}{M}} = \sqrt{\frac{k}{m + \frac{1}{3} m_{spring}}} .$$

Does this lead to a better comparison between model and experiment?

```
[> ms := .011; # spring has mass 11g
  M := m + 1/3 * ms; # "effective mass"
]
[> omega := sqrt(k/M); # predicted angular frequency
  f := evalf(omega/(2*Pi)); # predicted frequency
  T := 1/f; # predicted period
]>
```